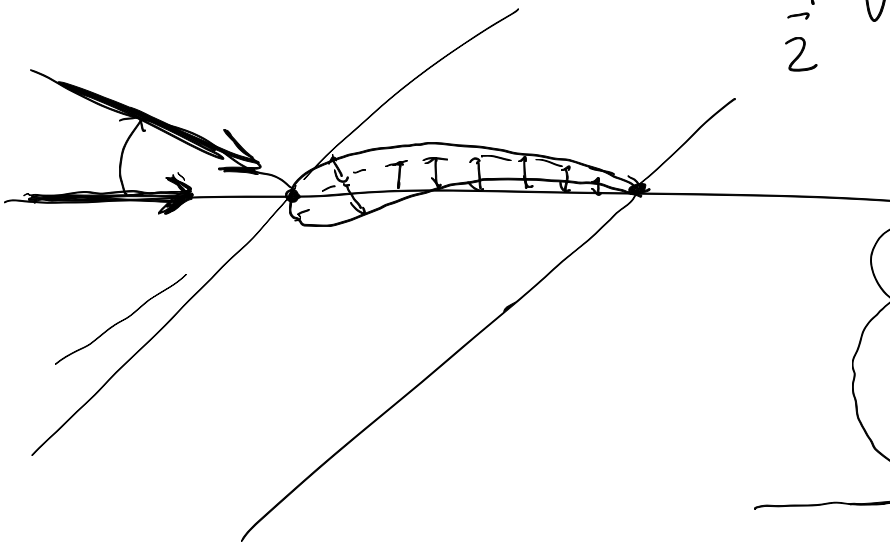
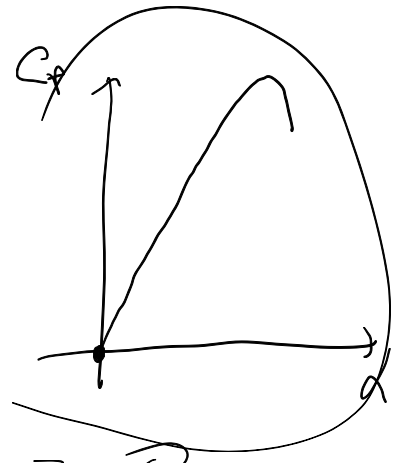


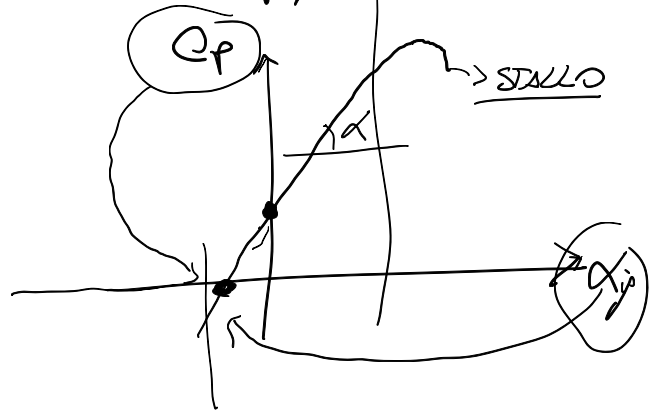


$d_{ij} = 0 \Rightarrow P = 0 \Rightarrow C_p = 0$

$$C_p = \frac{P}{\frac{1}{2} \rho V^2 S_f} = 0$$



$P \neq 0 \Rightarrow C_p \neq 0$



tend =

$C_p \propto \alpha^2$
 $C_p = q \alpha^2$

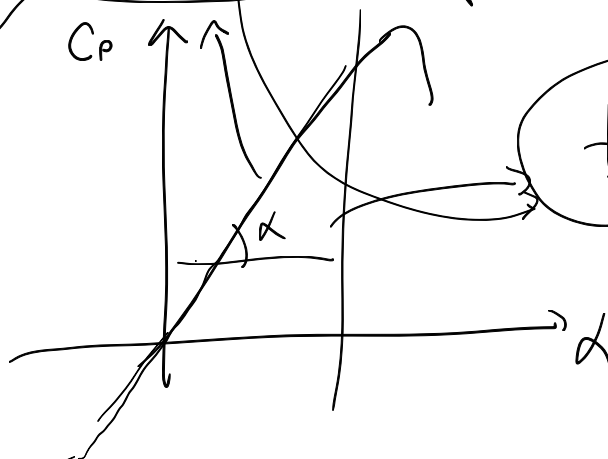
COEFFICIENTE ANGOLARE di PORTANZA

$\frac{dC_p}{d\alpha} =$

$C_p(\alpha)$

$C_p'(\alpha)$

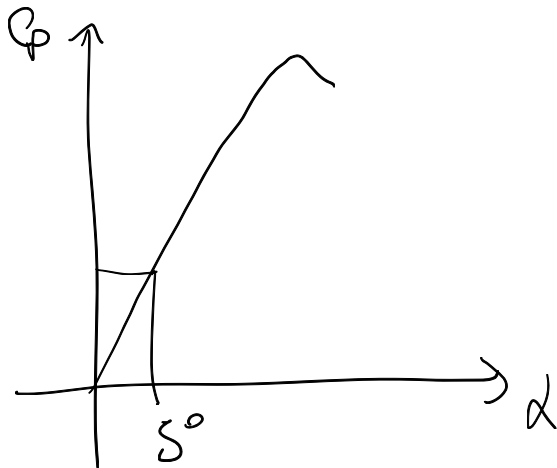
q



$tend = q$

$$\tan \alpha = q = 5.73$$

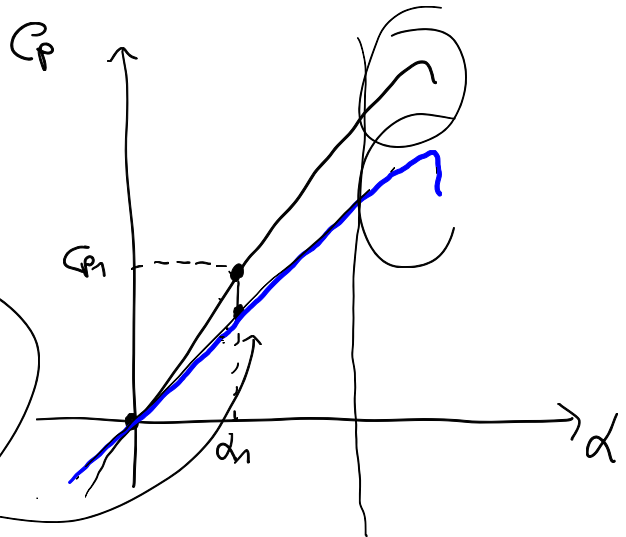
$$C_p = q \alpha = 5.73 \alpha$$



$$C_p = 5.73 \cdot 5^\circ \cdot \frac{\pi}{180}$$

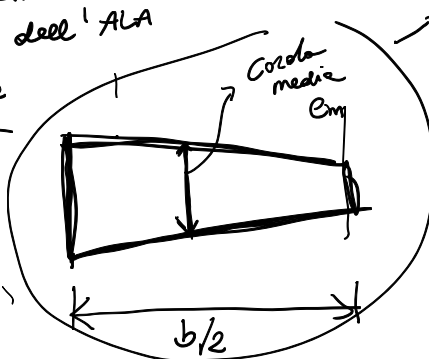
$$C_p = C_p' \alpha$$

$$C_p' = \frac{5.73}{1 + 5.73} \cdot \frac{\pi}{180}$$



λ : RAPPORTO di ASPETTO
= ALLUNGAMENTO dell'ALA

$$\lambda = \frac{b}{c_m} = \frac{b}{c_m} \cdot \frac{b}{b} = \frac{b^2}{S}$$



λ : secondo PRANDTL vale per un profilo di forme ellittiche → ha determinato analiticamente la resistenza indotta

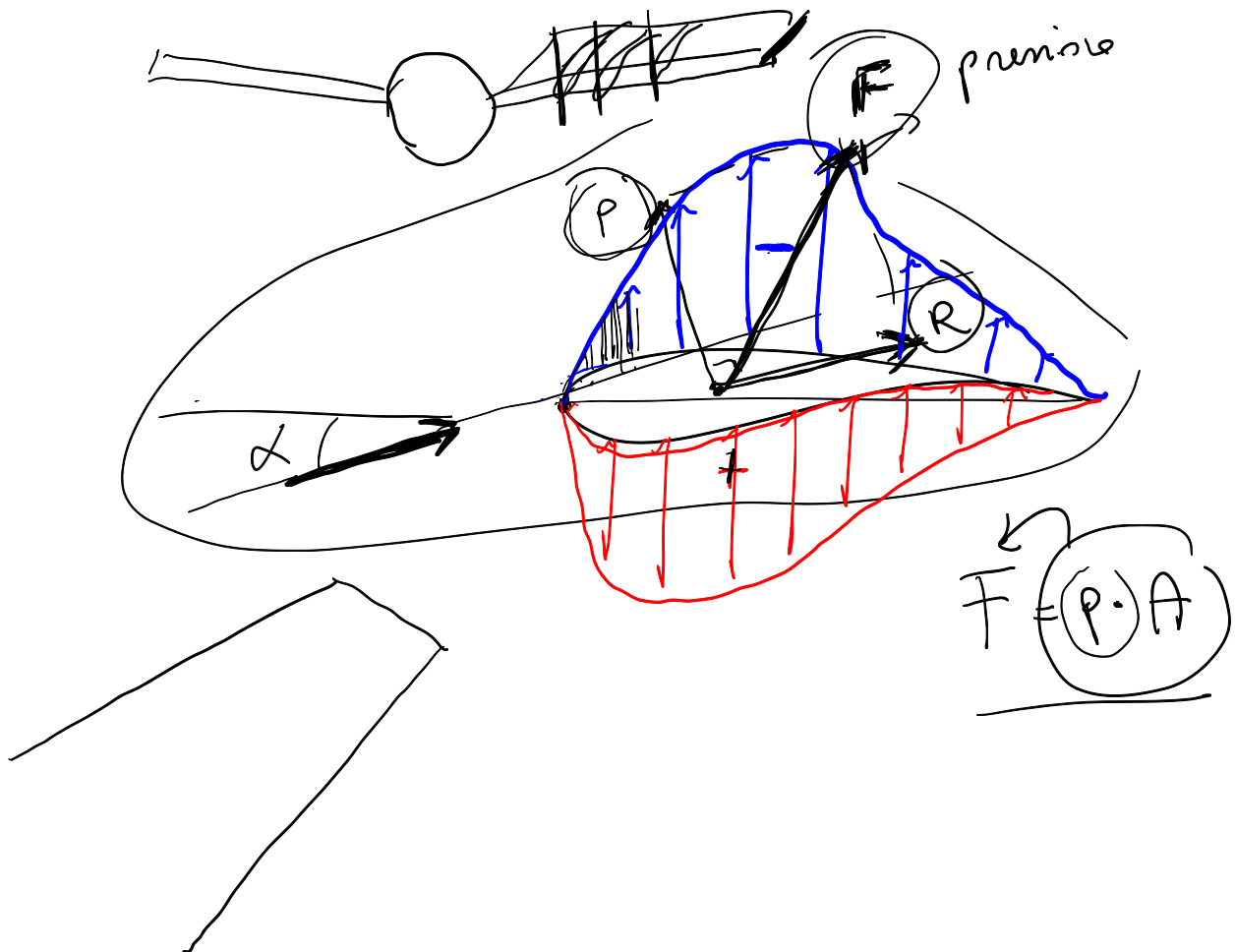
Se il profilo non è ellittico devo considerare

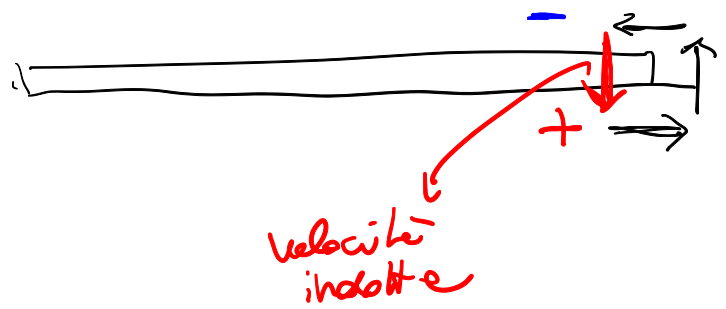
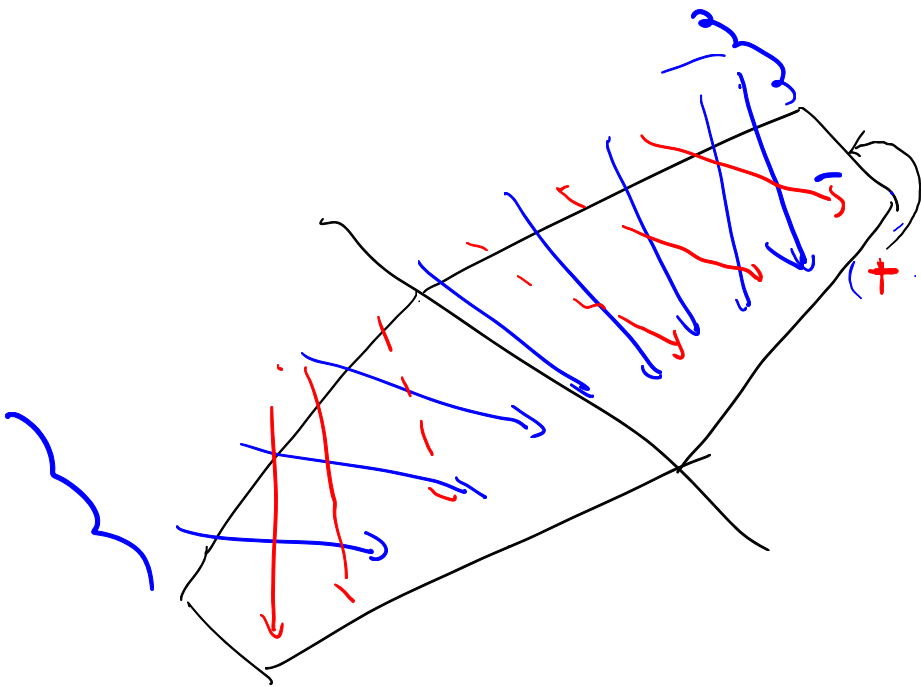
$$\lambda_{\text{eff}} = \mu \cdot \lambda$$

↓
EFFETTIVO

CORRISPONDENTE CORRETTIVO (di ANDERSON) che vale $\sim 0.8 \div 0.9$

ALA FINITA





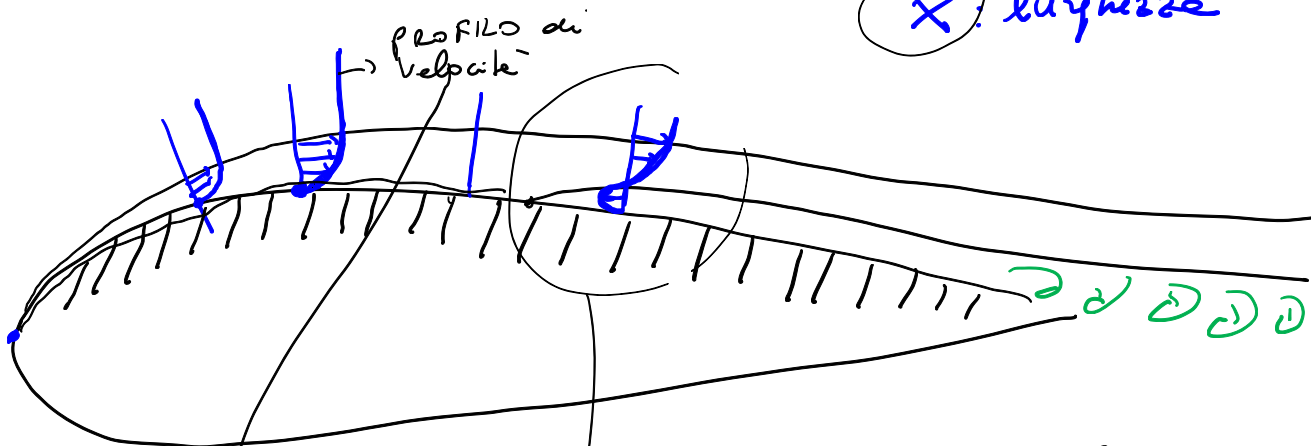
RESISTENZA INDOTTA

RESISTENZA di SCIA

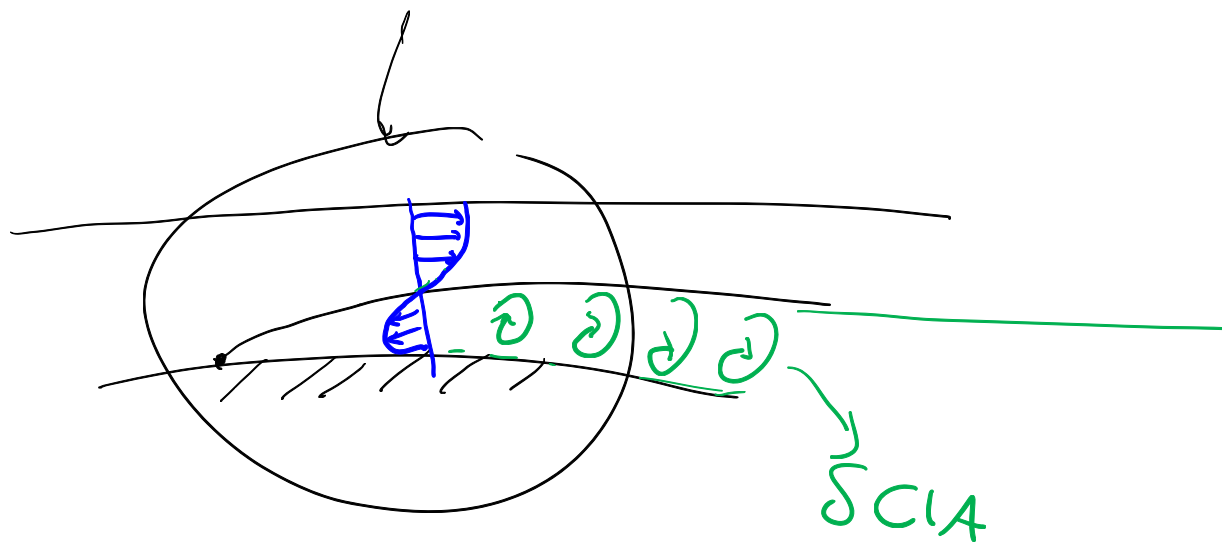
$$Re = \frac{V \cdot X}{\nu}$$

Re
NUMERO di REYNOLDS

ν : VISCOSITÀ CINEMATICA
 V : velocità
 X : lunghezza

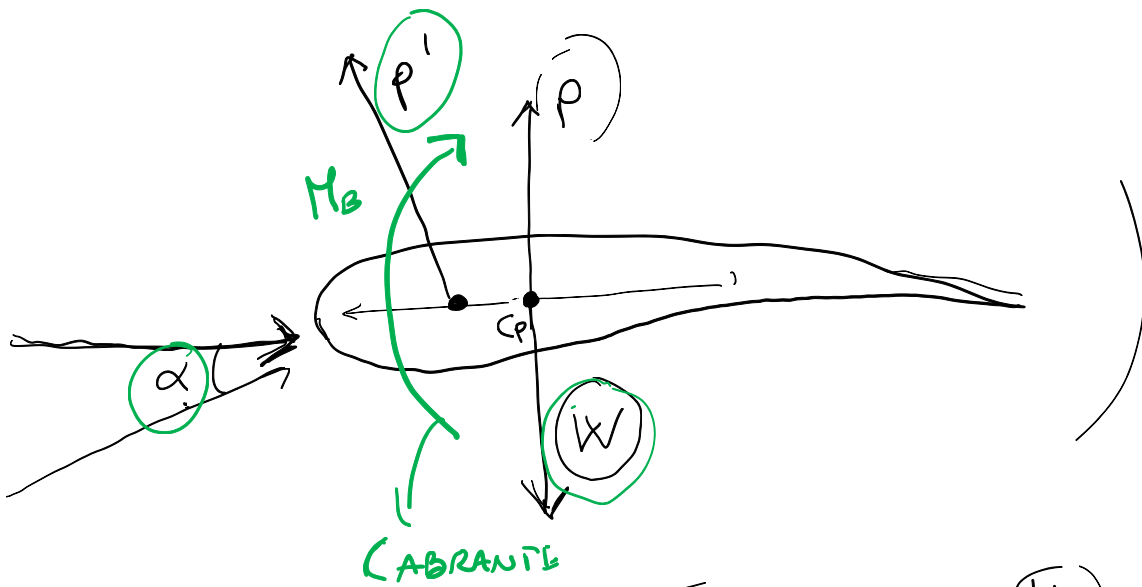


indica come varia la velocità delle particelle allontanandosi dal profilo



RESISTENZA di ATRITO $\rightarrow R_e$
 $f(R_e)$

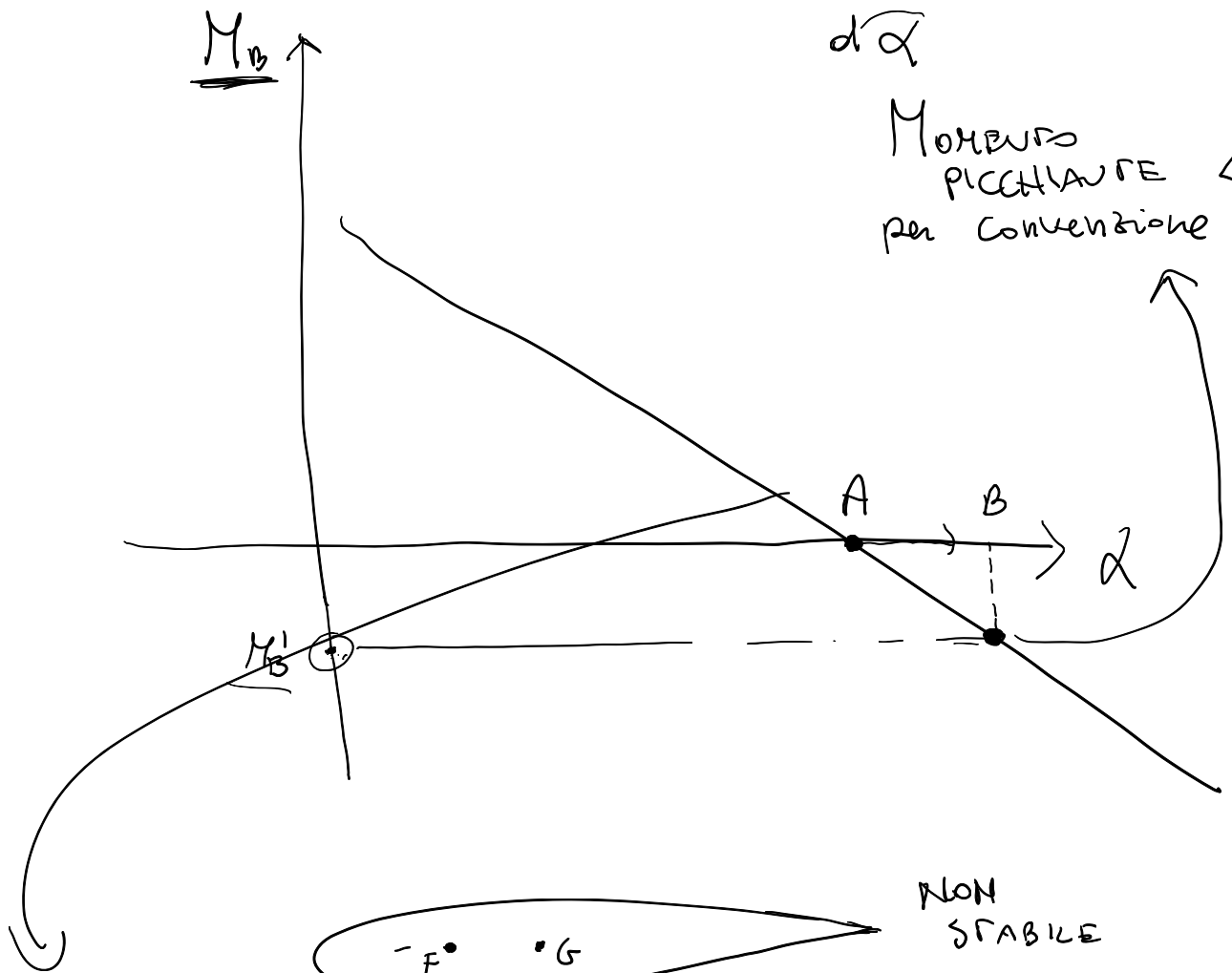
RESISTENZA $\left\{ \begin{array}{l} \text{ATRITO} \\ \rho \end{array} \right.$



(ABRANTE)

$$\frac{d(M_B)}{d\alpha} < 0$$

MOMENTO
PICCHIANTE < 0
per convenzione



NON
STABILE

Se G è posizionato davanti al fuoco.

